Chapter 7 - Center of Gravity and Centroids Reading: Chapter 7 - Pages 259 - 284

7-1 Introduction



The centroid, C, is a point defining the geometric center of an object.



The center of gravity, G, is defined as a point about which the entire weight of the body is assumed to be concentrated. The centroid coincides with the center of mass or the center of gravity only if the material of the body is homogenous (density or specific weight is constant throughout the body).



<u>Cylinder</u>

If an object has an axis of symmetry, then the centroid of the object lies on that axis.



In some cases, the centroid may not be located on the object. For the C shape (American Standard Channel) structural steel component shown above the centroid is given by the X-X and Y-Y centroidal axes.

7-2 Center of Gravity and Centroid of a Body

Center of Gravity (G)



The moment of W about O must be equal to the sum of the moments of the weight of all the particles about O.

Equating the moment about the z axis, we write

 $\bar{x} W = \Sigma x \Delta W$

Equating the moment about the x axis, we write

 $\bar{z} W = \Sigma z \Delta W$

Similarly, we can also write

 $\bar{y} W = \Sigma y \Delta W$

The following equations can be used for locating the center of gravity, G, of a solid body:

$$\overline{x} = \frac{\Sigma x \Delta W}{\Sigma \Delta W} \qquad \overline{y} = \frac{\Sigma y \Delta W}{\Sigma \Delta W} \qquad \overline{z} = \frac{\Sigma z \Delta W}{\Sigma \Delta W}$$
(7-1)

Centroid (C)

The center of mass of a geometric object of uniform density.

Locating the Centroid of a Volume Homogeneous body (uniform)

γ = weight per unit volume (constant)

 $\Delta W = \gamma \Delta v$ (weight of a particle)

 $W = \gamma v$ (weight of the entire body)

Substituting in Equation 7-1 and dividing through by γ , we obtain

$$\overline{x} = \frac{\Sigma x \Delta V}{\Sigma \Delta V} \qquad \overline{y} = \frac{\Sigma y \Delta V}{\Sigma \Delta V} \qquad \overline{z} = \frac{\Sigma z \Delta V}{\Sigma \Delta V}$$
(7-2)

Centroids of Volumes of Common Shapes

Formulas for computing the volumes and locations of centroids of common geometric shapes, such as cylinders, spheres, hemispheres, circular cones, and so on, have been determined mathematically and are listed in Table 7-1 (see next page).

Centroid of Composite Volumes

A volume can be divided into several component volumes of shapes is called a composite volume. The coordinates of the centroid C (\bar{x} , \bar{y} , \bar{z}) of a composite volume may be computed from the following equations:

$$\overline{x} = \frac{\Sigma V x}{\Sigma V} = \frac{V_1 x_1 + V_2 x_2 + V_3 x_3 + \cdots}{V_1 + V_2 + V_3 + \cdots}$$

$$\overline{y} = \frac{\Sigma V y}{\Sigma V} = \frac{V_1 y_1 + V_2 y_2 + V_3 y_3 + \cdots}{V_1 + V_2 + V_3 + \cdots}$$

$$\overline{z} = \frac{\Sigma V z}{\Sigma V} = \frac{V_1 z_1 + V_2 z_2 + V_3 z_3 + \cdots}{V_1 + V_2 + V_3 + \cdots}$$

(7-3)



TABLE 7–1 Centroids of Volumes of Common Shapes

7–2 Locate the centroid of a body consisting of the cylinder and circular cone shown in Fig. P7–2.



FIGURE P7–2

7-4 The mallet in Fig. P7–4 has a head made of steel and a cylindrical handle made of wood. The handle fits tightly into a hole over the entire width of the head. Locate the center of gravity of the mallet given $\gamma_{st} = 490 \text{ lb/ft}^3$, and $\gamma_{wd} = 40 \text{ lb/ft}^3$.



FIGURE P7-4



7-3 Experimental Determination of the Center of Gravity



$$\Sigma M_A = -W\overline{x} + W_B b = 0$$

From which we get

$$\overline{x} = \frac{W_B}{W}b \tag{7-4}$$



Substituting \overline{x} from Equation 7–4 and solving for \overline{y} , we get

$$\overline{y} = \frac{W_B b \cos\theta - W_B' b \cos\theta}{W \sin\theta}$$

or

$$\overline{y} = \frac{b}{W \tan\theta} \left(W_B - W_B' \right) \tag{7-5}$$

7-4 Centroid of an Area

<u>Centroid, C</u> Defines the geometric center of an object

Uniform Body – density is constant (γ) also called, specific weight

C, coincides with G, if the body is uniform.

<u>Symmetry</u>

If the shape (body) has an axis of symmetry, the centroid, C, of the shape will lie along that axis.



I-SECTION

Centroid of an Area

Reference Axis – the location of the centroid of a shape is determined with respect to a given reference axis.

Centroid of a Composite Area

$$\overline{x} = \frac{\Sigma A x}{\Sigma A} = \frac{A_1 x_1 + A_2 x_2 + A_3 x_3 + A_4 x_4}{A_1 + A_2 + A_3 + A_4}$$

$$\overline{y} = \frac{\Sigma A y}{\Sigma A} = \frac{A_1 y_1 + A_2 y_2 + A_3 y_3 + A_4 y_4}{A_1 + A_2 + A_3 + A_4}$$
(7-7)

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TABLE 7–2 Centroids of Areas of Common Shapes

Example 1. Locate the centroid of the plane area shown. Use the given reference axis.

Solution.

- 1. Break the composite shape into common geometric areas.
- 2. Choose a Reference Axis or use the given Reference Axis
- 3. Construct a table as shown below.

Shape	Area (ft²)	x (ft)	Ax (ft³)	y (ft)	Ay (ft³)
Σ					

4. Find \bar{x} and \bar{y}

Example 2. Locate the centroid of the plane area shown. Use the given reference axis.

Shape	Area (ft²)	x (ft)	Ax (ft³)	y (ft)	Ay (ft³)
Σ					

Example 3.

Locate the centroid of the built-up structural steel section with respect to the given reference axis.

- X

Structural Steel Properties can be found in Appendix A of the text book. The following tables can be found in the course notes on pages 146 and 147.

Table A-1(a) Properties of Selected W Shapes (Wide-Flange Sections) Table A-3(a) Properties of C Shapes (Channels)

Shape	Area (in²)	x (ft)	Ax (in³)	y (ft)	Ay (in³)
Σ					

TABLE A-l(a) (Continued) Properties of Selected W Shapes (Wide-Flange Sections): U.S. Customary Units

			Web	Fla	nge		Elastic Properties						Plastic	
Desig- nation	Area	Depth	Thick- ness	Width	Thick- ness	Ì	Axis <i>x-x</i>		P	Axis y—y	7	Modulus		
(in. \times lb/ft)	A (in. ²)	d (in.)	t _w (in.)	b _f (in.)	t _f (in.)	I (in. ⁴)	S (in. ³)	r (in.)	<i>I</i> (in. ⁴)	S (in.³)	r (in.)	Z _X (in. ³)	Z _Y (in. ³)	
	21.8 20.0 17.9 15.6 12.6 11.2 10.0 8.85	14.17 14.04 13.89 13.92 13.66 14.10 13.98 13.84	0.450 0.415 0.375 0.370 0.305 0.310 0.285 0.270	10.070 10.035 9.995 8.060 7.995 6.770 6.745 6.730	0.785 0.720 0.645 0.660 0.530 0.515 0.455 0.385	796 723 640 541 428 385 340 291	112 103 92.2 77.8 62.7 54.6 48.6 42.0	6.04 6.01 5.98 5.89 5.82 5.87 5.83 5.73	134 121 107 57.7 45.2 26.7 23.3 19.6	26.6 24.2 21.5 14.3 11.3 7.88 6.91 5.82	2.48 2.46 2.45 1.92 1.89 1.55 1.53 1.49	126 115 102 87.1 69.6 61.5 54.6 47.3	40.6 36.9 32.8 22.0 17.3 12.1 10.6 8.99	
$\begin{array}{cccc} \mathbb{W}12 \times & 87 \\ \times & 65 \\ \times & 53 \\ \times & 40 \\ \times & 35 \\ \times & 30 \\ \times & 22 \end{array}$	25.6 19.1 15.6 11.8 10.3 8.79 6.48	12.53 12.12 12.06 11.94 12.50 12.34 12.31	0.515 0.390 0.345 0.295 0.300 0.260 0.260	12.125 12.000 9.995 8.005 6.560 6.520 4.030	0.810 0.605 0.575 0.515 0.520 0.440 0.425	740 533 425 310 285 238 156	118 87.9 70.6 51.9 45.6 38.6 25.4	5.38 5.28 5.23 5.13 5.25 5.21 4.91	241 174 95.8 44.1 24.5 20.3 4.66	39.7 29.1 19.2 11.0 7.47 6.24 2.31	3.07 3.02 2.48 1.93 1.54 1.52 0.847	132 96.8 77.9 57.5 51.2 43.1 29.3	60.4 44.1 29.1 16.8 11.5 9.56 3.66	
W10 × 112 × 100 × 88 × 77 × 60 × 49 × 45 × 39 × 33 × 22	32.9 29.4 25.9 22.6 17.6 14.4 13.3 11.5 9.71 6.49	11.36 11.10 10.84 10.60 10.22 9.98 10.10 9.92 9.73 10.17	0.755 0.680 0.605 0.530 0.420 0.340 0.350 0.315 0.290 0.240	10.415 10.340 10.265 10.190 10.080 10.000 8.020 7.985 7.960 5.750	1.250 1.120 0.990 0.870 0.680 0.560 0.620 0.530 0.435 0.360	716 623 534 455 341 272 248 209 170 118	126 112 98.5 85.9 66.7 54.6 49.1 42.1 35.0 23.2	4.66 4.60 4.54 4.39 4.35 4.32 4.27 4.19 4.27	236 207 179 154 116 93.4 53.4 45.0 36.6 11.4	45.3 40.0 34.8 30.1 23.0 18.7 13.3 11.3 9.20 3.97	2.68 2.65 2.63 2.60 2.57 2.54 2.01 1.98 1.94 1.33	147 130 113 97.6 74.6 60.4 54.9 46.8 38.8 26.0	69.2 61.0 53.1 45.9 35.0 28.3 20.3 17.2 14.0 6.10	
$\begin{array}{cccc} \mathbb{W8} \times & 67 \\ \times & 58 \\ \times & 48 \\ \times & 40 \\ \times & 35 \\ \times & 31 \\ \times & 28 \\ \times & 24 \\ \times & 21 \\ \times & 18 \end{array}$	19.7 17.1 14.1 11.7 10.3 9.13 8.25 7.08 6.16 5.26	9.00 8.75 8.50 8.25 8.12 8.00 8.06 7.93 8.28 8.14	0.570 0.510 0.400 0.360 0.310 0.285 0.285 0.245 0.245 0.250 0.230	8.280 8.220 8.110 8.070 8.020 7.995 6.535 6.495 5.270 5.250	0.935 0.810 0.685 0.560 0.495 0.435 0.465 0.400 0.400 0.330	272 228 184 146 127 110 98.0 82.8 75.3 61.9	60.4 52.0 43.3 35.5 31.2 27.5 24.3 20.9 18.2 15.2	3.72 3.65 3.61 3.53 3.51 3.47 3.45 3.42 3.42 3.49 3.43	88.6 75.1 60.9 49.1 42.6 37.1 21.7 18.3 9.77 7.97	21.4 18.3 15.0 12.2 10.6 9.27 6.63 5.63 3.71 3.04	2.12 2.10 2.08 2.04 2.03 2.02 1.62 1.61 1.26 1.23	70.2 59.8 49.0 39.8 34.7 30.4 27.2 23.2 20.4 17.0	32.7 27.9 22.9 18.5 16.1 14.1 10.1 8.57 5.69 4.66	

			177.1				4		1			
Desig-	Area	Depth	Thick-	Width	ange Average		Axis <i>x-x</i>			Axis v–t	7	Cen-
nation			ness		Thick-							troid
in. $ imes$ lb/ft	A	d	t _w	b _f	t _f	[S	г	<i>I</i>	S	г	7
	(in.²)	(in.)	(in.)	(in.)	(in.)	(in.4)	(in. ³)	(in.)	(in. ⁴)	(in. ³)	(in.)	(in.)
C15 × 50	14.7	15.00	0.716	3.716	0.650	404	53.8	5.24	11.0	3.78	0.867	0.798
× 40	11.8	15.00	0.520	3.520	0.650	349	46.5	5.44	9.23	3.37	0.886	0.777
× 33.9	9.96	15.00	0.400	3.400	0.650	315	42.0	5.62	8.13	3.11	0.904	0.787
C12 × 30	8.82	12.00	0.510	3.170	0.501	162	27.0	4.29	5.14	2.06	0.763	0.674
× 25	7.35	12.00	0.387	3.047	0.501	144	24.1	4.43	4.47	1.88	0.780	0.674
× 20.7	6.09	12.00	0.282	2.942	0.501	129	21.5	4.61	3.88	1.73	0.799	0.698
C10 × 30	8.82	10.00	0.673	3.033	0.436	103	20.7	3.42	3.94	1.65	0.669	0.649
× 25	7.35	10.00	0.526	2.886	0.436	91.2	18.2	3.52	3.36	1.48	0.676	0.617
× 20	5.88	10.00	0.379	2.739	0.436	78.9	15.8	3.66	2.81	1.32	0.692	0.606
× 15.3	4.49	10.00	0.240	2.600	0.436	67.4	13.5	3.87	2.28	1.16	0.713	0.634
C 9×20 ×15 ×13.4	5.88 4.41 3.94	9.00 9.00 9.00	0.448 0.285 0.233	2.648 2.485 2.433	0.413 0.413 0.413	, 60.9 51.0 47.9	13.5 11.3 10.6	3.22 3.40 3.48	2.42 1.93 1.76	1.17 1.01 0.962	0.642 0.661 0.669	0.583 0.586 0.601
C 8×18.75	5.51	8.00	0.487	2.527	0.390	44.0	11.0	2.82	1.98	1.01	0.599	0.565
×13.75	4.04	8.00	0.303	2.343	0.390	36.1	9.03	2.99	1.53	0.854	0.615	0.553
×11.5	3.38	8.00	0.220	2.260	0.390	32.6	8.14	3.11	1.32	0.781	0.625	0.571
$ \begin{array}{c} \overbrace{7 \times 14.75} \\ \times 12.25 \\ \times 9.8 \end{array} $	4.33	7.00	0.419	2.299	0.366	27.2	7.78	2.51	1.38	0.779	0.564	0.532
	3.60	7.00	0.314	2.194	0.366	24.2	6.93	2.60	1.17	0.703	0.571	0.525
	2.87	7.00	0.210	2.090	0.366	21.3	6.08	2.72	0.968	0.625	0.581	0.540
C 6×13	3.83	6.00	0.437	2.157	0.343	17.4	5.80	2.13	1.05	0.642	0.525	0.514
×10.5	3.09	6.00	0.314	2.034	0.343	15.2	5.06	2.22	0.866	0.564	0.529	0.499
×8.2	2.40	6.00	0.200	1.920	0.343	13.1	4.38	2.34	0.693	0.492	0.537	0.511
C 5×9	2.64	5.00	0.325	1.885	0.320	8.96	3.56	1.83	0.632	0.450	0.489	0.478
×6.7	1.97	5.00	0.190	1.750	0.320	7.49	3.00	1.95	0.479	0.378	0.493	0.484
$\begin{array}{c} C & 4 \times 7.25 \\ \times 5.4 \end{array}$	2.13	4.00	0.321	1.721	0.296	4.59	2.29	1.47	0.433	0.343	0.450	0.459
	1.59	4.00	0.184	1.584	0.296	3.85	1.93	1.56	0.319	0.283	0.449	0.457
$\begin{array}{c} C & 3 \times 6 \\ \times 5 \\ \times 4.1 \end{array}$	1.76	3.00	0.356	1.596	0.273	2.07	1.38	1.08	0.305	0.268	0.416	0.455
	1.47	3.00	0.258	1.498	0.273	1.85	1.24	1.12	0.247	0.233	0.410	0.438
	1.21	3.00	0.170	1.410	0.273	1.66	1.10	1.17	0.197	0.202	0.404	0.436

TABLE A-3(a)Properties of C Shapes (American Standard
Channels): U.S. Customary Units

Example 4.

Locate the centroid of the built-up structural steel section with respect to the given reference axis.

Shape	Area (in²)	x (ft)	Ax (in³)	y (ft)	Ay (in³)
Σ					

TABLE A-4(a) (Continued) Properties of Selected L Shapes

(Steel Angles): U.S. Customary Units

Size a Thickn	nd	Weight	Area	Axis x–x				Axis y–y				Axis z–z	
(in.))	(lb/ft)	A (in.²)	[(in. ⁴)	S (in. ³)	r (in.)	у (in.)	[(in. ⁴)	S (in. ³)	r (in.)	<i>x</i> (in.)	г (in.)	tan a
L 4×4	$\times \frac{3}{4}$	18.5	5.44	7.67	2.81	1.19	1.27	7.67	2.81	1.19	1.27	0.778	1.000
	$\times \frac{5}{8}$	15.7	4.61	6.66	2.40	1.20	1.23	6.66	2.40	1.20	1.23	0.779	1.000
	$\times \frac{1}{2}$	12.8	3.75	5.56	1.97	1.22	1.18	5.56	1.97	1.22	1.18	0.782	1.000
	$\times \frac{3}{8}$	9.8	2.86	4.36	1.52	1.23	1.14	4.36	1.52	1.23	1.14	0.788	1.000
	$\times \frac{5}{16}$	8.2	2.40	3.71	1.29	1.24	1.12	3.71	1.29	1.24	1.12	0.791	1.000
	$\times \frac{1}{4}$	6.6	1.94	3.04	1.05	1.25	1.09	3.04	1.05	1.25	1.09	0.795	1.000
$L 4 \times 3\frac{1}{2}$	$\times \frac{1}{2}$	11.9	3.50	5.32	1.94	1.23	1.25	3.79	1.52	1.04	1.00	0.722	0.750
	$\times \frac{3}{8}$	9.1	2.67	4.18	1.49	1.25	1.21	2.95	1.17	1.06	0.955	0.727	0.755
	$\times \frac{5}{16}$	7.7	2.25	3.56	1.26	1.26	1.18	2.55	0.994	1.07	0.932	0.730	0.757
	$\times \frac{1}{4}$	6.2	1.81	2.91	1.03	1.27	1.16	2.09	0.808	1.07	0.909	0.734	0.579
$L 4 \times 3$	$\times \frac{1}{2}$	11.1	3.25	5.05	1.89	1.25	1.33	2.42	1.12	0.864	0.827	0.639	0.543
	$\times \frac{3}{8}$	8.5	2.48	3.96	1.46	1.26	1.28	1.92	0.866	0.879	0.782	0.644	0.551
	$\times \frac{5}{16}$	7.2	2.09	3.38	1.23	1.27	1.26	1.65	0.734	0.887	0.759	0.647	0.554
	$\times \frac{1}{4}$	5.8	1.69	2.77	1.00	1.28	1.24	1.36	0.599	0.896	0.736	0.651	0.558
$L 3\frac{1}{2} \times 3\frac{1}{2}$	$\times \frac{3}{8}$	8.5	2.48	2.87	1.15	1.07	1.01	2.87	1.15	1.07	1.01	0.687	1.000
	$\times \frac{5}{16}$	7.2	2.09	2.45	0.976	1.08	0.990	2.45	0.976	1.08	0.990	0.690	1.000
5	$\times \frac{1}{4}$	5.8	1.69	2.01	0.794	1.09	0.968	2.01	0.794	1.09	0.968	0.694	1.000
$L 3\frac{1}{2} \times 3$	$\times \frac{3}{8}$	7.9	2.30	2.72	1.13	1.09	1.08	1.85	0.851	0.897	0.830	0.625	0.721
	$\times \frac{5}{16}$	6.6	1.93	2.33	0.954	1.10	1.06	1.58	0.722	0.905	0.808	0.627	0.724
	$\times \frac{1}{4}$	5.4	1.56	1.91	0.776	1.11	1.04	1.30	0.589	0.914	0.785	0.631	0.727
$L 3\frac{1}{2} \times 2\frac{1}{2}$	$\times \frac{3}{8}$	7.2	2.11	2.56	1.09	1.10	1.16	1.09	0.592	0.719	0.660	0.537	0.496
	$\times \frac{5}{16}$	6.1	1.78	2.19	0.927	1.11	1.14	0.939	0.504	0.727	0.637	0.540	0.501
	$\times \frac{1}{4}$	4.9	1.44	1.80	0.755	1.12	1.11	0.777	0.412	0.735	0.614	0.544	0.506
L 3×3	$\times \frac{1}{2}$	9.4	2.75	2.22	1.07	0.898	0.932	2.22	1.07	0.898	0.932	0.584	1.000
	$\times \frac{3}{8}$	7.2	2.11	1.76	0.833	0.913	0.888	1.76	0.833	0.913	0.888	0.587	1.000
	$\times \frac{5}{16}$	6.1	1.78	1.51	0.707	0.922	0.865	1.51	0.707	0.922	0.865	0.589	1.000
	$\times \frac{1}{4}$	4.9	1.44	1.24	0.577	0.930	0.842	1.24	0.577	0.930	0.842	0.592	1.000
,	$\times \frac{3}{16}$	3.71	1.09	0.962	0.441	0.939	0.820	0.962	0.441	0.939	0.820	0.596	1.000
$L 3 \times 2\frac{1}{2}$	$\times \frac{8}{3}$	6.6	1.92	1.66	0.810	0.928	0.956	1.04	0.581	0.736	0.706	0.522	0.676
	$\times \frac{1}{4}$	4.5	1.31	1.17	0.561	0.945	0.911	0.743	0.404	0.753	0.661	0.528	0.684
	$\times \frac{3}{16}$	3.39	0.996	0.907	0.430	0.954	0.888	0.577	0.310	0.761	0.638	0.533	0.688
L 3×2	$\times \frac{8}{3}$	5.9	1.73	1.53	0.781	0.940	1.04	0.543	0.371	0.559	0.539	0.430	0.428
	$\times \frac{5}{16}$	5.0	1.46	1.32	0.664	0.948	1.02	0.470	0.317	0.567	0.516	0.432	0.435
	$\times \frac{1}{4}$	4.1	1.19	1.09	0.542	0.957	0.993	0.392	0.260	0.574	0.493	0.435	0.440
	$\times \frac{3}{16}$	3.07	0.902	0.842	0.415	0.966	0.970	0.307	0.200	0.583	0.470	0.439	0.446

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7-5

General Types of Distributed Line Loads

Distributed Load

A distributed load occurs whenever the load applied to a body is not concentrated at a point.

The total resultant over the entire length of the beam is: $P = \Sigma q\Delta x = \Sigma \Delta A = A$ Thus, the resultant of a distributed line load is equal to the area of the loading diagram.

The location of the resultant P along the beam may be determined by requiring that the moment of P about O be equal to the sum of the moments of the loads q Δx over the entire beam about O.

From the Equivalent Resultant diagram: $\Sigma M_{o} = P d = \Sigma (q\Delta x)x = \Sigma (\Delta A)x = A \bar{x} = P \bar{x}$

Thus, $Pd = P \bar{x}$ $d = \bar{x}$ Line of action of the resultant P passes through the centroid of the area

Example 1. Determine the reactions at the supports of the beams for the loading shown.

Solution.

The loading diagram is divided into a parabolic spandrel, rectangular area, and triangular area.

